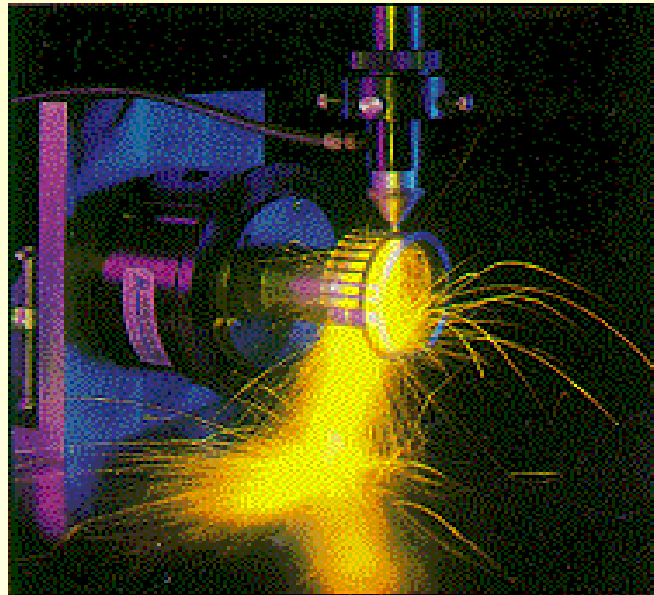


# *A Numerical Investigation of Laser Heating Including the Phase Change Process in Relation to Laser Drilling*



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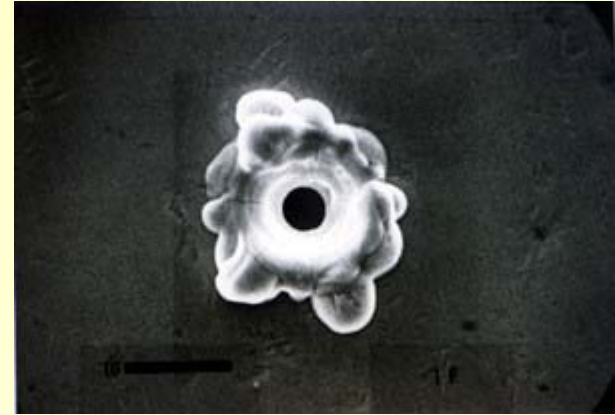


# *Overview:*

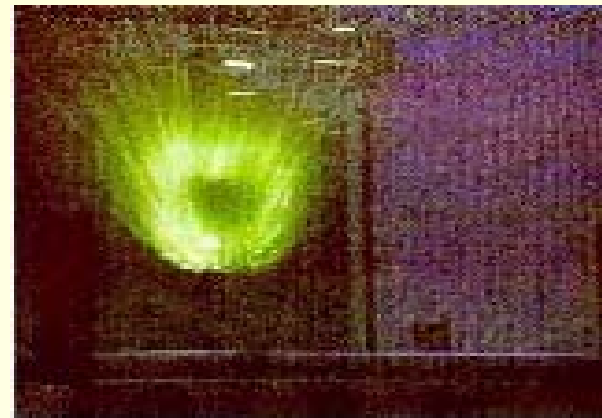
- **Introduction**
- **Laser material interaction**
- **Mathematical modeling**
- **Numerical solution**
- **Results & discussion**
- **Conclusions**

# *Why Laser Drilling?*

- **Precision**
- **Robustness**
- **Versatility**
- **No physical contact**

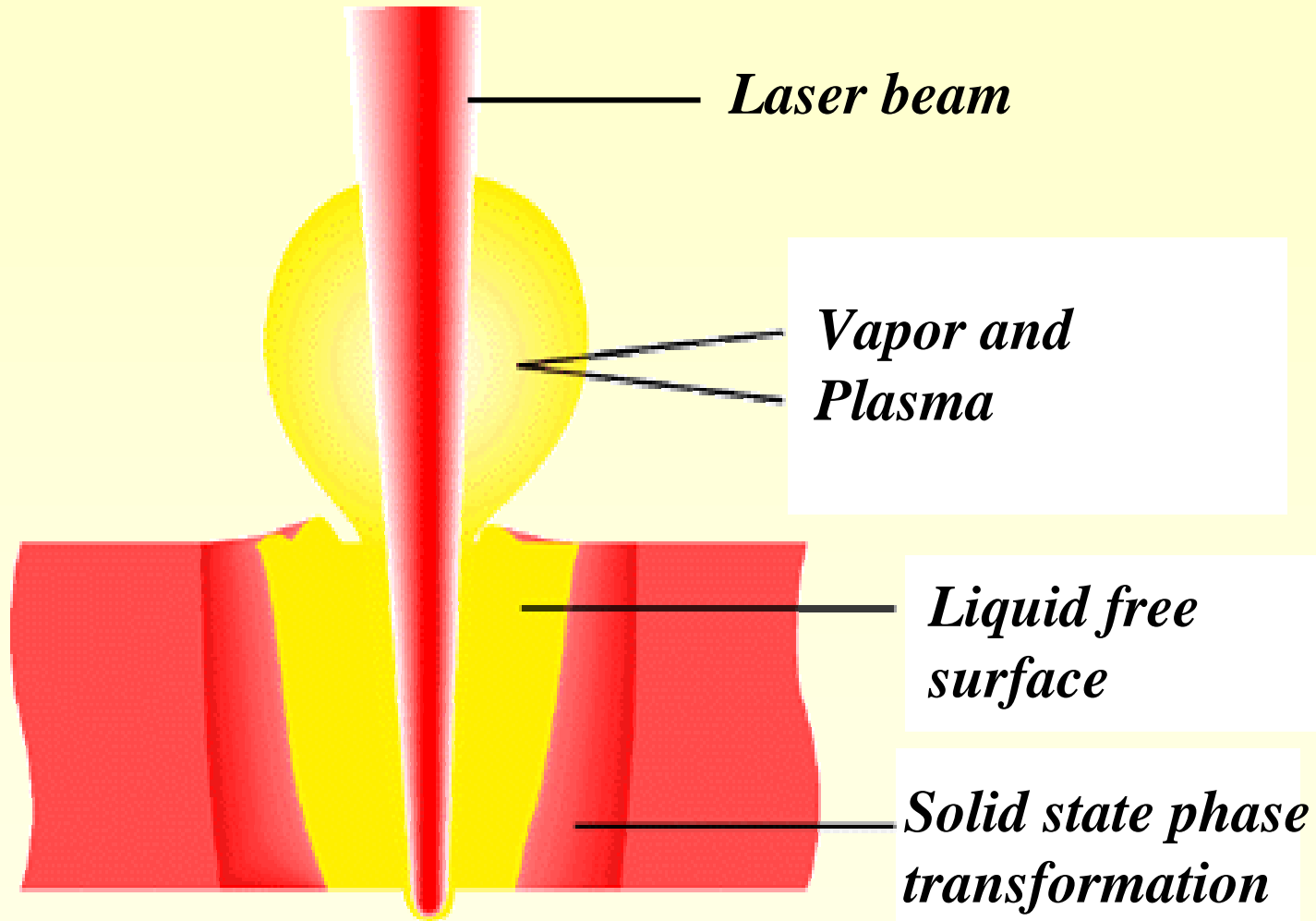


*A 7  $\mu\text{m}$  dia. hole drilled by Laser*



*6 in. dia. hole with high energy Laser beam*

# *Laser Material Interaction:*



*Schematic view of laser material interaction*

## *Interaction Physics:*

- **When a laser strikes the material, electrons in the near surface region absorb the energy.**
- **Electrons collide with the lattice and transfer this energy to the bulk of the material (electron relaxation).**
- **The temperature of the bulk starts rising.**
- **If the laser has enough energy the temperature can reach to the melting or even the boiling point.**
- **When material starts ablating from the surface a cavity is formed.**

## *Mathematical Modeling:*

- **If the laser pulse length or the heating period is more than the electron relaxation time a Fourier heating model is applicable.**
- **The laser acts as a source term in the heating model.**
- **Because of the phase change it is a moving boundary problem.**
- **The model also needs to accommodate the shape change of the domain with surface ablation.**

# *Heating Models:*

## **1. Classical Phase Change Model-Stefan Problem.**

**Good for analytical solution.**

**Cannot account for ablation.**

## **2. Energy method.**

**Good for numerical solution.**

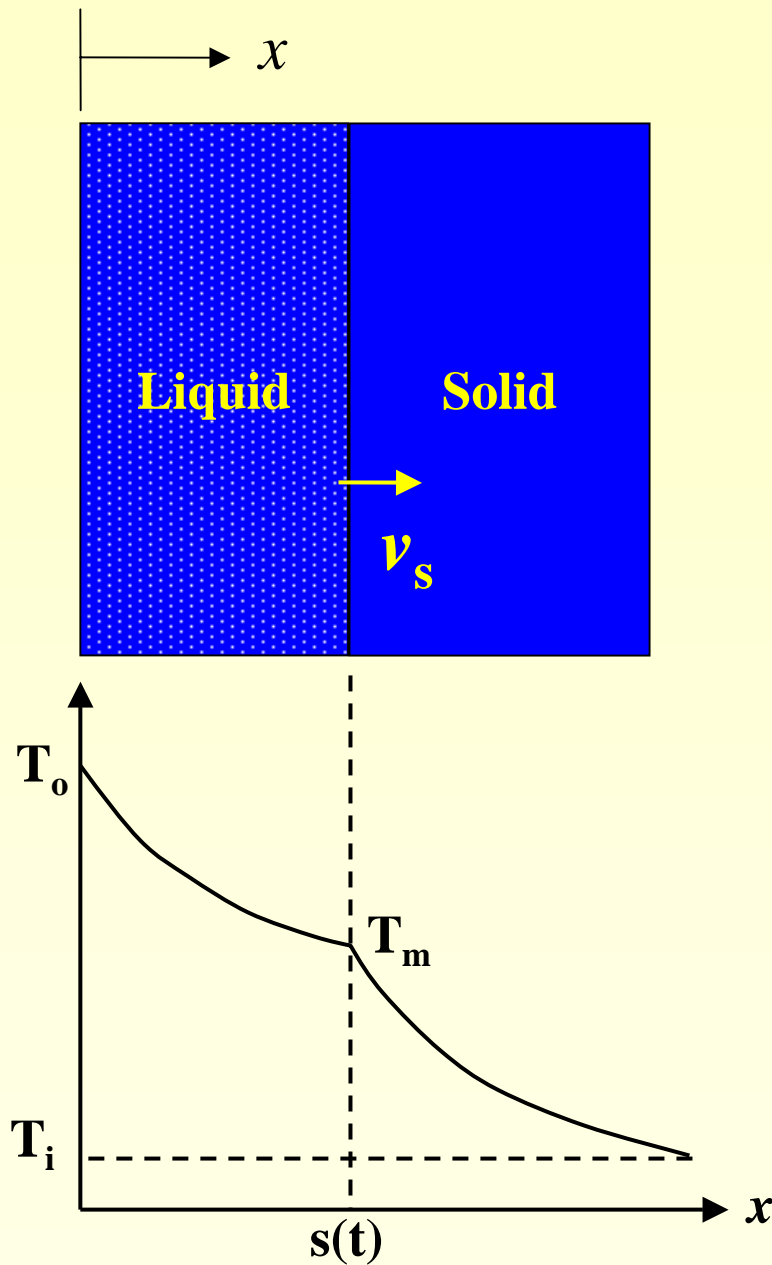
**Can take care of ablation.**

# *Stefan Problem:*

## **Assumptions:**

- **Unsteady heat transfer.**
- **Solid and liquid phases are separated by a sharp interface.**
- **The Fourier equation is applicable on the solid and liquid phases separately.**
- **The energy balance is being applied at the interface.**





$T_m$  = Melting temperature

$v_s$  = Interface velocity

$T_0$  = Boundary temperature

$T_i$  = Initial temperature

$s(t)$  = Interface position

*Phase change from solid to liquid with sharp interface*

**In solid phase:**

$$\rho_s c_{ps} \frac{\partial T_s}{\partial t} = k_s \frac{\partial^2 T_s}{\partial x^2} \quad 0 \leq x \leq s(t)$$

**In liquid phase:**

$$\rho_l c_{pl} \frac{\partial T_l}{\partial t} = k_l \frac{\partial^2 T_l}{\partial x^2} \quad s(t) \leq x \leq \infty$$

**At the interface:**

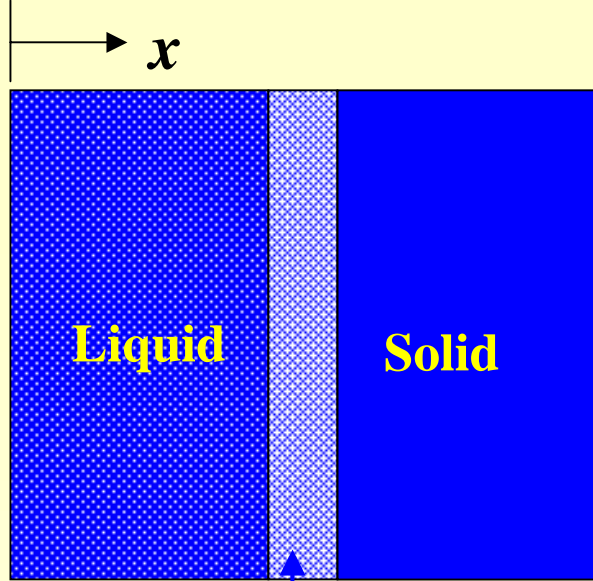
$$\left[ \begin{array}{l} \text{Conduction heat} \\ \text{flux in positive } x \\ \text{direction through} \\ \text{liquid phase.} \end{array} \right] + \left[ \begin{array}{l} \text{Rate of heat} \\ \text{addition during} \\ \text{melting per unit} \\ \text{area of Interface.} \end{array} \right] = \left[ \begin{array}{l} \text{Conduction heat} \\ \text{flux in positive } x \\ \text{direction through} \\ \text{solid phase.} \end{array} \right]$$

or  $k_s \frac{\partial T_s}{\partial x} - k_l \frac{\partial T_l}{\partial x} = \rho_s L v_s \quad \text{at} \quad x = s(t), \quad t > 0$

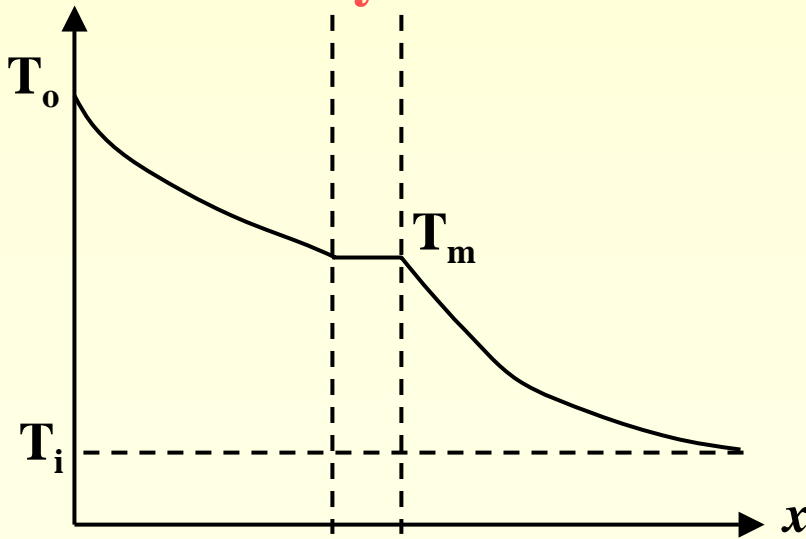
# *Energy Method:*

## **Assumptions:**

- **Unsteady heat transfer.**
- **Solid-liquid or liquid-gas phases are separated by a region of considerable thickness called the ‘mushy zone’.**
- **The mushy zone is the mixture of two phases at the melting or boiling temperature.**
- **The energy balance is being applied on the mushy zone.**



Mushy zone



*Phase change from solid to liquid for energy method.*

**Laser drilling is axisymmetric heating.**

**For solid and liquid phases;**

$$\rho c_p \frac{\partial T}{\partial t} = \frac{k}{r} \frac{\partial}{\partial r} \left( r \frac{\partial T}{\partial r} \right) + k \frac{\partial^2 T}{\partial z^2} + S_o$$

**Where;**

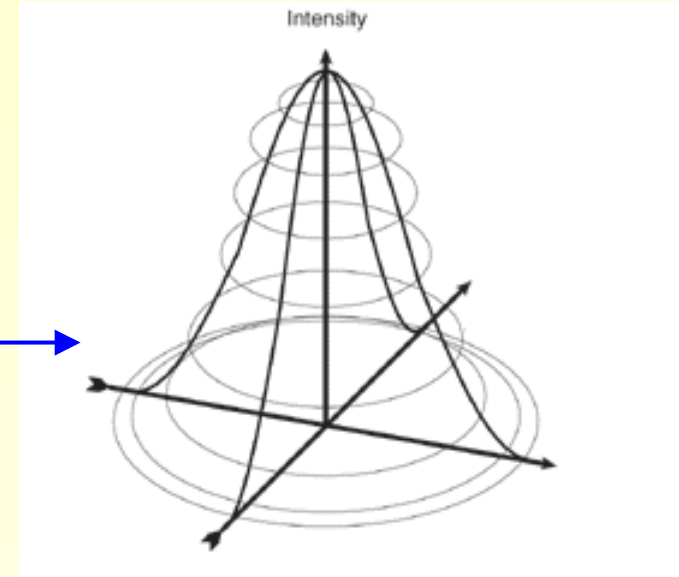
$$S_o = I_o \delta (1 - r_f) \exp(-\delta z) \exp\left(-\frac{r^2}{a^2}\right)$$

$I_o = \text{Intensity}$

$\delta = \text{Absorption depth}$

$r_f = \text{Surface reflectivity}$

$a = \text{Gaussian parameter}$



***Laser intensity  
distribution***

## Energy balance for solid-liquid mushy zone;

$$\rho L_m \frac{\partial x_m}{\partial t} = \frac{k}{r} \frac{\partial}{\partial r} \left( r \frac{\partial T}{\partial r} \right) + k \frac{\partial^2 T}{\partial z^2} + S_o$$

## Energy balance for liquid-gas mushy zone;

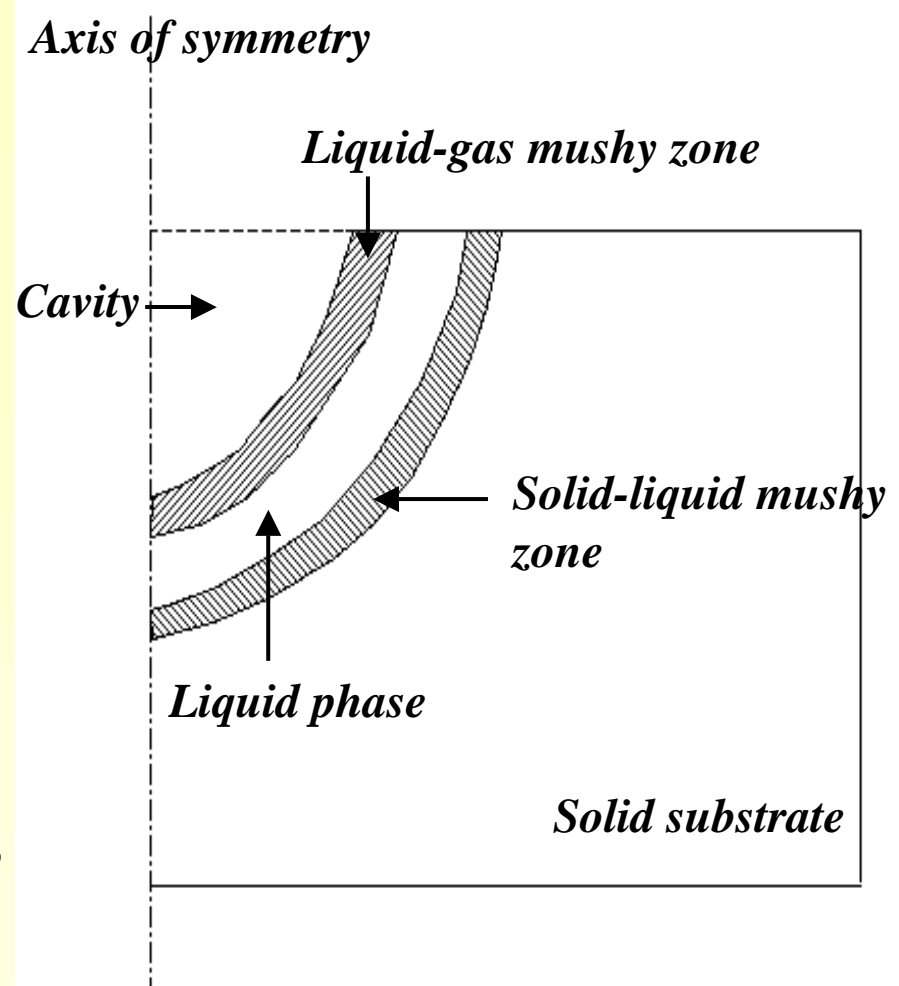
$$\rho L_b \frac{\partial x_b}{\partial t} = \frac{k}{r} \frac{\partial}{\partial r} \left( r \frac{\partial T}{\partial r} \right) + k \frac{\partial^2 T}{\partial z^2} + S_o$$

$L_m$  = Latent heat of fusion

$x_m$  = Liquid mass fraction

$L_b$  = Latent heat of boiling

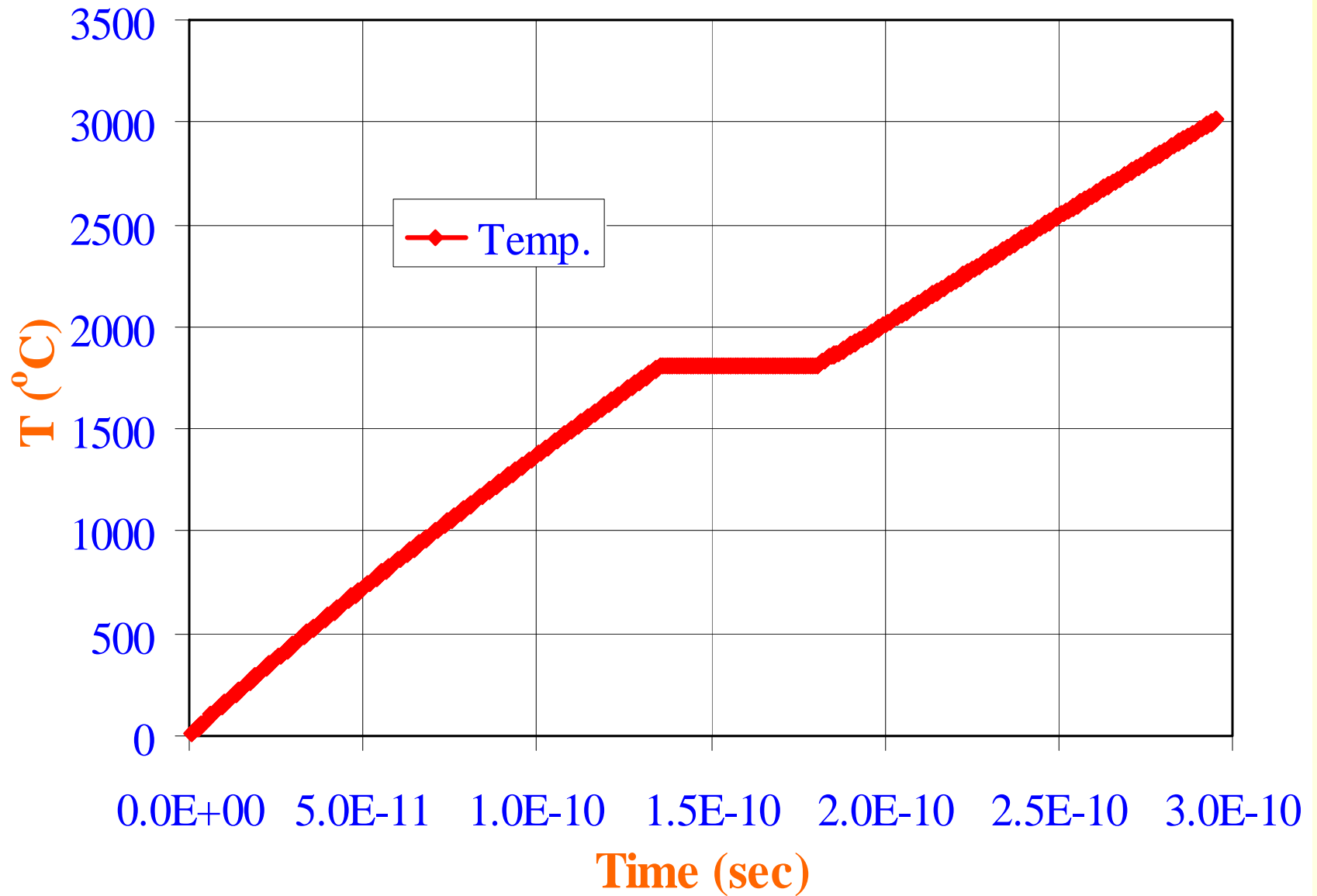
$x_b$  = Vapor mass fraction



*Axisymmetric heating and surface ablation with two mushy zones*

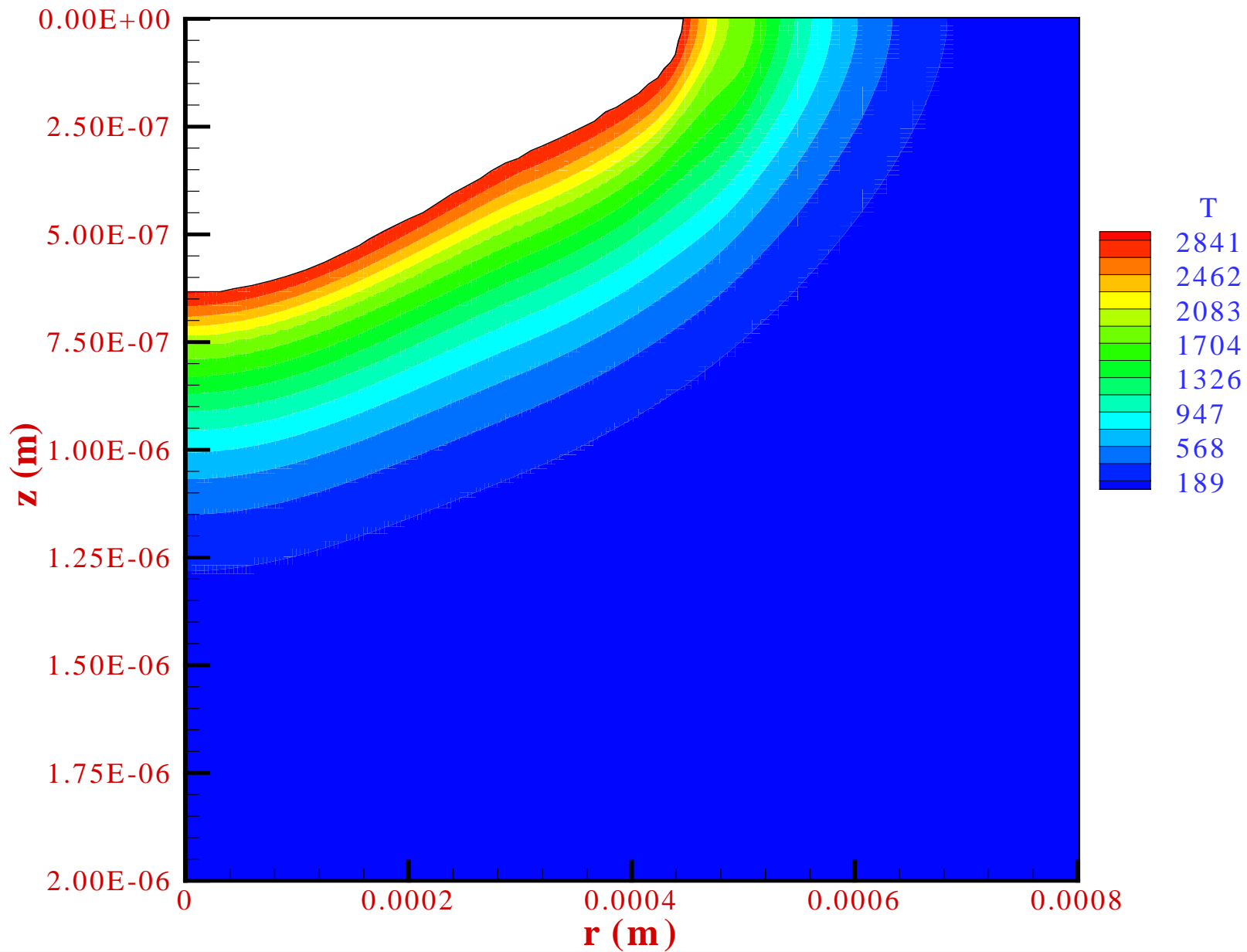
## *Numerical Solution:*

- **The model equations are discretized using a finite volume approach and solved in explicit time marching fashion.**
- **Liquid-gas mushy zone equation also determines the change in the domain shape with the ablation.**

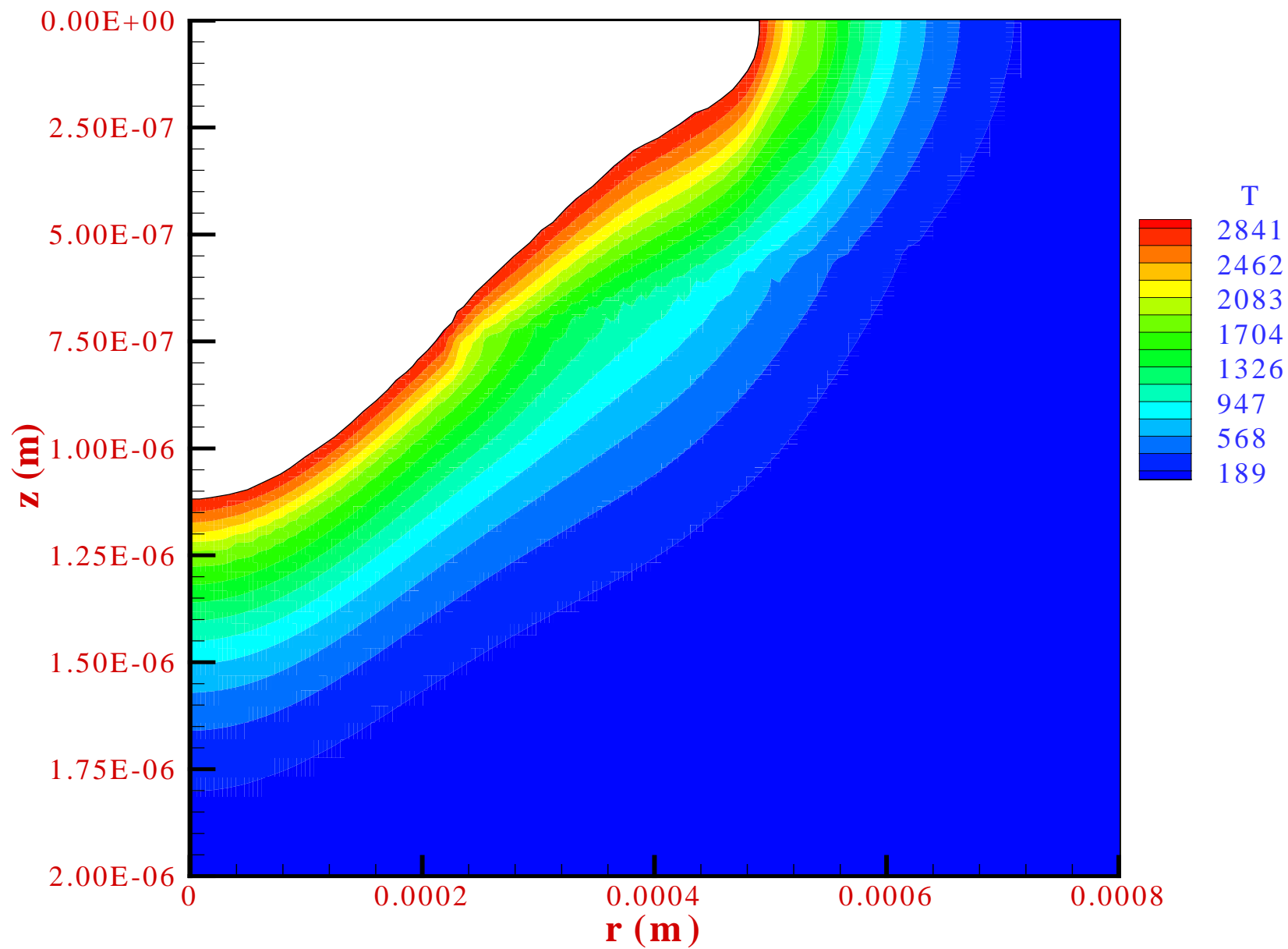


*Temporal variation of temperature at the beam centre*

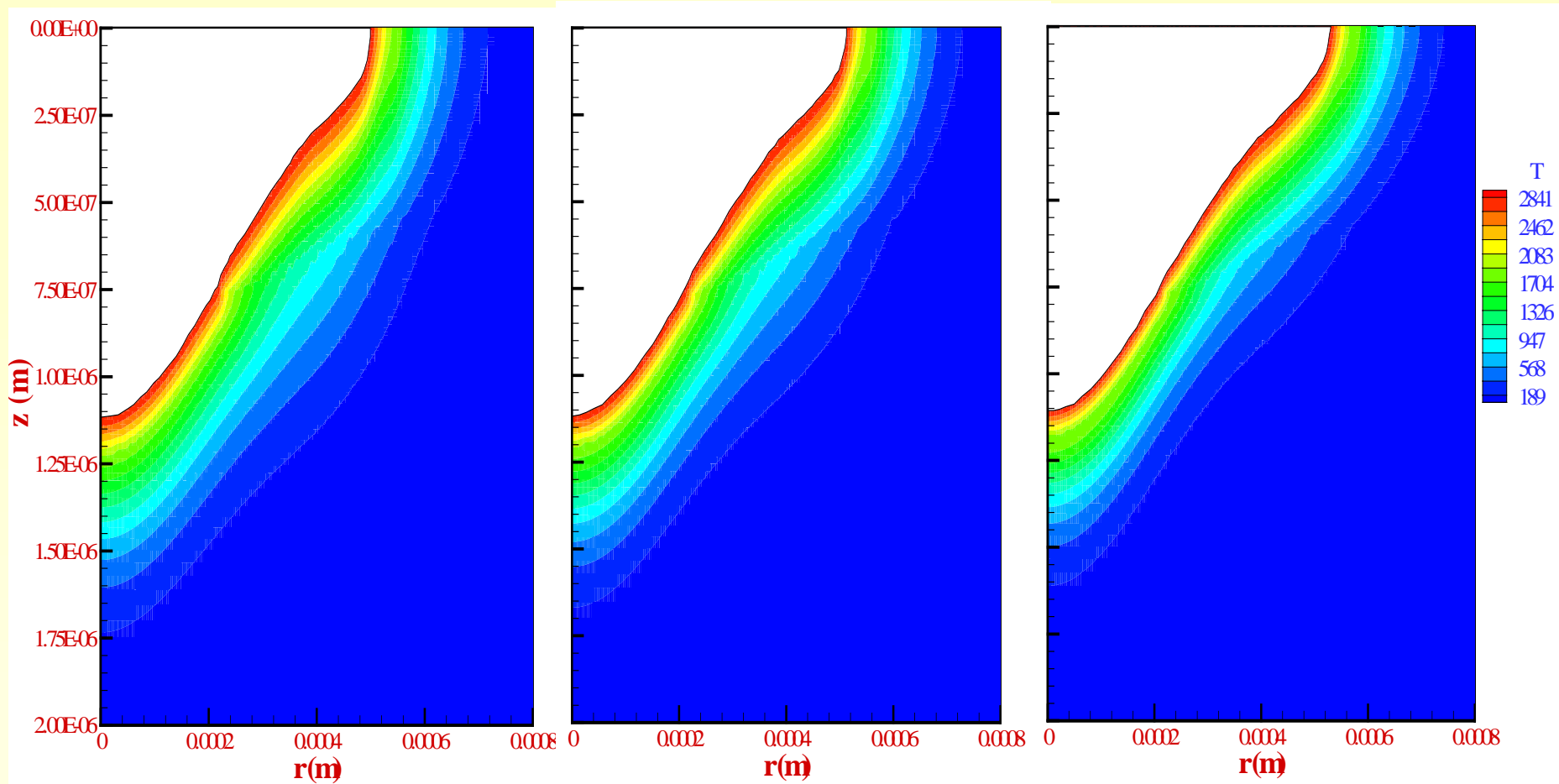




*Temperature contours in the substrate at 4 ns*



*Temperature contours in the substrate at 8 ns*

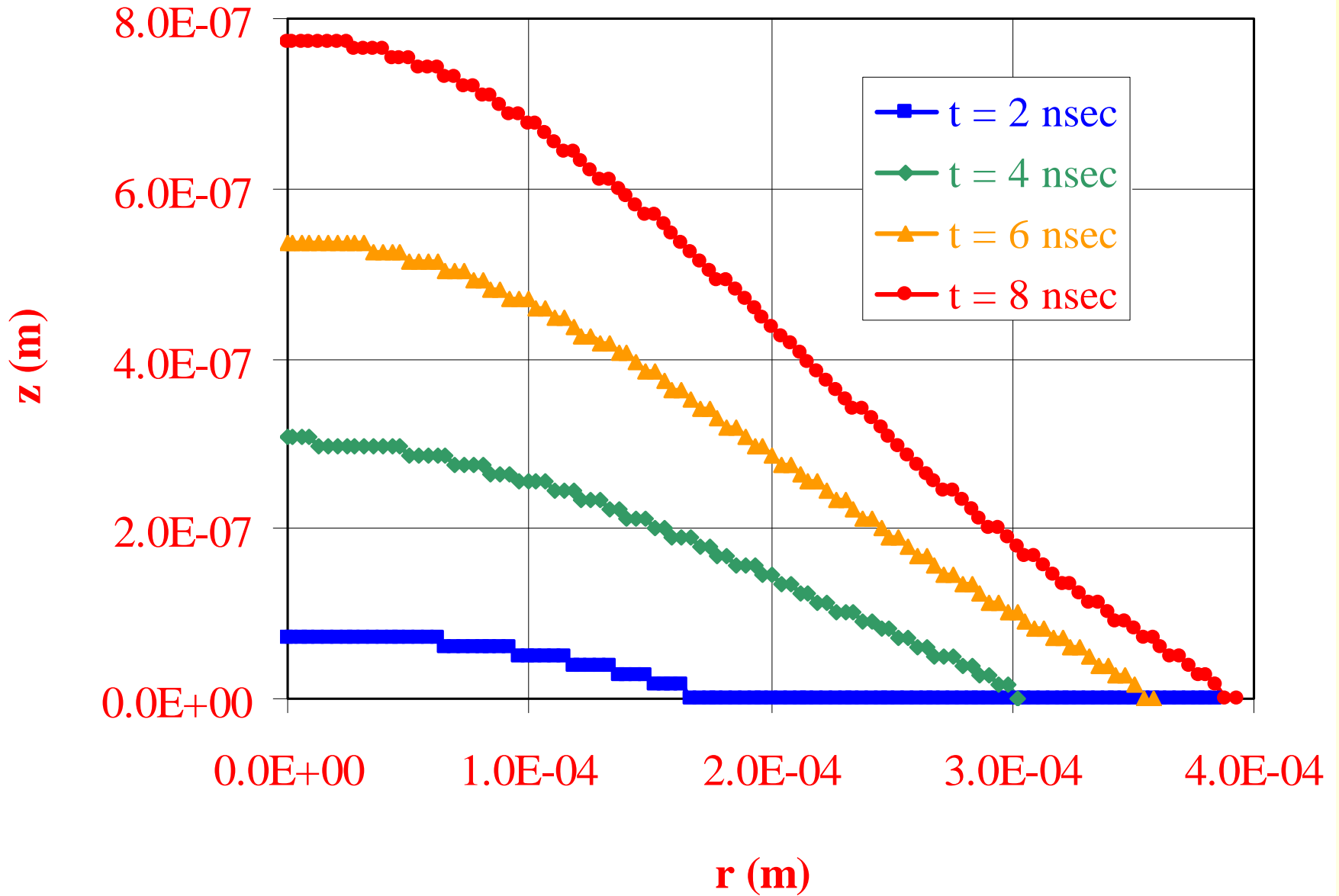


$$9.3 \times 10^{12} \text{ W/m}^2, 6 \text{ ns}$$

$$14 \times 10^{12} \text{ W/m}^2, 4 \text{ ns}$$

$$28 \times 10^{12} \text{ W/m}^2, 2 \text{ ns}$$

*Effect of beam intensity on the heat-affected zone*



*Development of the drilled hole geometry*

## *Conclusions:*

- **The energy method can capture the phase change process.**
- **With high energy input only a very small amount of heat diffuses in the substrate because of the ablations.**
- **The depth of the heat-affected zone is independent of the pulse length.**
- **The heat-affected zone can be reduced by using a higher pulse intensity.**

*Thank you*